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(54) **Dual thermal and ultraviolet curable powder coatings**

(57) Opaquely pigmented or thick filmed powder coatings for heat sensitive substrates, such as wood, wood composites, for example, medium density fiber board, and plastics, that can be fully cured, especially near the substrate, through the incorporation of a dual cure system in the powder comprising a thermal initiator, such as a peroxide, along with a UV initiator. The UV initiator cures the surface, while the thermal initiator cures at the substrate. Surprisingly, virtually no pregelation occurs during the heated melt and flow out step prior to UV curing. Consequently, the hardened film finish formed on the surface exhibits exceptional smooth-

ness which is comparable to that of traditional UV curable powders. The hardened film finish is also fully cured throughout and exhibits exceptional adhesion to the substrate which cannot be achieved with traditional UV curable powders that have been pigmented. Although the dual cure system includes a thermal aspect, these powder coatings are especially suited for coating heat sensitive substrates. The dual thermal and UV curable powders still cure at significantly lower temperatures and significantly faster rates than traditional heat curable powders to make them safe for coating heat sensitive substrates.

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**Description****Field of the Invention**

5 The present invention relates to powder coatings and more particularly to opaquely pigmented or thick filmed ultraviolet (UV) radiation curable powder coatings that can be cured not only at the surface, but also down through the coating to the substrate. Full cure can be obtained despite the presence of opaque pigments or thick films that normally impede the penetration of radiation in the coating and, consequently, inhibit cure below the surface. This is accomplished by incorporating a thermal initiator in the UV curable powder coatings together with the usual UV initiator.

10 Surprisingly, the presence of a thermal initiator does not detract from the exceptional smoothness of the hardened film finishes. The dual thermal and UV curable powder coatings of the present invention are especially suited for coating over heat sensitive substrates, such as wood and plastic, since these coatings cure at faster speeds and/or lower temperatures, reducing the potentially damaging heat load on the substrate.

**Background of the Invention**

Powder coatings, which are dry, finely divided, free flowing, solid materials at room temperature, have gained considerable popularity in recent years over liquid coatings for a number of reasons. For one, powder coatings are user and environmentally friendly materials, since they are virtually free of harmful fugitive organic solvent carriers that

20 are normally present in liquid coatings. Powder coatings, therefore, give off little, if any, volatile materials to the environment when cured. This eliminates the solvent emission problems associated with liquid coatings, such as air pollution and dangers to the health of workers employed in coating operations.

Powder coatings are also clean and convenient to use. They are applied in a clean manner over the substrate, since they are in dry, solid form. The powders are easily swept up in the event of a spill and do not require special cleaning and spill containment supplies, as do liquid coatings. Working hygiene is, thus, improved. No messy liquids

25 are used that adhere to worker's clothes and to the coating equipment, which leads to increased machine downtime and clean up costs.

Powder coatings are essentially 100% recyclable. Over sprayed powders can be fully reclaimed and recombined with the powder feed. This provides very high coating efficiencies and also substantially reduces the amount of waste generated. Recycling of liquid coatings during application is not done, which leads to increased waste and hazardous waste disposal costs.

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Despite their many advantages, powder coatings are generally not employed in coating heat sensitive substrates, such as wood and plastic. Heat sensitive substrates demand lower cure temperatures, preferably below 250°F, to avoid significant substrate degradation and/or deformation. Lower cure temperatures are not possible with traditional heat curable powders. Unsuccessful attempts have been made to coat heat sensitive substrates with traditional powders.

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For instance, when wood composites, e.g., particle board, fiber board, and other substrates that contain a significant amount of wood, are heated to the high cure temperatures required for traditional powders, the residual moisture and resinous binders present in the wood composites for substrate integrity are caused to invariably evolve from the substrate. Outgassing of the volatiles during curing results in severe blisters, craters, pinholes, and other surface defects in the hardened film finish. Furthermore, overheating causes the wood composites to become brittle, friable, charred, and otherwise worsened in physical and chemical properties. This is unacceptable from both a film quality and product quality viewpoint.

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Low temperature UV curable powders have recently been proposed for coating heat sensitive substrates. UV powders still require exposure to heat, which is above either the glass transition temperature ( $T_g$ ) or melt temperature ( $T_m$ ), to sufficiently melt and flow out the powders into a continuous, smooth, molten film over the substrate prior to radiation curing. However, the heat load on the substrate is significantly reduced, since UV powders are formulated to melt and flow out at much lower temperatures than traditional powder coatings, typically on the order of about 200°F. Therefore, UV powders only need to be exposed to enough low temperature heat required to flow out the powders into a smooth molten film.

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Curing or hardening of UV powders is accomplished by exposing the molten film to light from a UV source, such as a mercury UV lamp, which rapidly cures the film. Since the crosslinking reactions are triggered with UV radiation rather than heat, this procedure allows the powder coatings to be cured more quickly and at much lower temperatures than traditional heat curable powders.

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Another significant advantage of UV curable powders is that the heated flow out step is divorced from the UV cure step. This enables the UV powders to completely outgas substrate volatiles during flow out and produce exceptionally smooth films prior to the initiation of any curing reactions. Accordingly, the film finishes created with UV powders are known to have extraordinary smoothness.

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One drawback is that opaque pigmentation of UV curable powders is known to be problematic. Opaque pigments

inherently absorb, reflect, or otherwise interfere with the transmittance of UV light through the pigmented coating, and, consequently, impede the penetration of UV light into the lower layers of the pigmented film during curing. Pigmented UV powders, when cured, can still provide exceptionally smooth film finishes with good surface cure properties, including good solvent resistance. However, pigmented UV powders are not able to be adequately cured down through the film to the underlying substrate. As a result, pigmented UV powder coatings exhibit poor through cure properties, including poor pencil hardness, poor adhesion, and poor flexibility. Clear UV powder formulations which are applied as thicker films greater than about 2 mils present similar curing problems. Most UV curable powder coatings produced today are formulated as thin clear coats for wood and metals without pigmentation.

EP Publication No. 0 636 669 A2 to DSM, N.V. dated Feb. 1, 1995 discloses UV or electron beam radiation curable powder coatings which can be applied to heat sensitive substrates, such as wood, *e.g.*, medium density fiber board, and plastic. The UV powders of EP 0 636 669 A2 contain: a) an unsaturated resin from the group of (semi)crystalline or amorphous unsaturated polyesters, unsaturated polyacrylates, and mixtures thereof, with unsaturated polyesters derived from maleic acid and fumaric acid being especially preferred; b) a crosslinking agent selected from an oligomer or polymer having vinyl ether, vinyl ester or (meth)acrylate functional groups, with vinyl ether functional oligomers being especially preferred, such as divinyl ether functionalized urethanes; and, c) a photoinitiator for UV or electron beam radiation cure, in which the equivalent ratio of polymer unsaturation to crosslinker unsaturation is preferably 1:1. However, the UV powders of EP 0 636 669 A2 are practically limited to being formulated as unpigmented, *i.e.*, clear, coatings, as demonstrated in Example 1. A similar clear coat UV powder based on an unsaturated polyester, an allyl ether ester crosslinker, and a hydroxyketone photoinitiator is disclosed in Example 2 of International Publication No. WO 93/19132 to DSM, N.V. dated September 30, 1993.

K.M. Biller and B. MacFadden (Herberts Powder Coatings), *UV-Curable Powders: A Marriage Of Compliant Coatings*, Industrial Paint & Powder, pp. 22-25 (July 1996) and K.M. Biller and B. MacFadden (Herberts Powder Coatings) *UV-Curable Powder Coatings: The Perfect Marriage of Compliant Coatings*, Radtech North America 1996 Conference, pp. 437-445 (April 28-May 2, 1996), suggest the incorporation of special solid UV initiators which are designed to activate despite the presence of various pigmentations. Presumably, these special UV initiators have some ability to absorb UV light at wavelengths above the reflectance of the pigments.

F.M. Witt and E.S. de Jong (DSM, N.V.), *Powder Coatings On Heat Sensitive Substrates*, presented at the DSM, N.V. seminar held in Amsterdam (27-28 March 1996), disclose that some success has been achieved in the laboratory with pigmented UV curable powder coating formulations based on a binder which comprises a blend of: a) an unsaturated polyester resin, *e.g.*, an unsaturated polyester derived from maleic acid; and, b) a vinyl ether functionalized polyurethane crosslinking agent. This binder is similar to that described in the aforementioned EP 0 636 669 A2. In these formulations, a special class of UV photoinitiators especially suited for pigmented UV coatings are used, *e.g.*, bis-acylphosphineoxides and a 75/25 blend of a hydroxyketone (Irgacure 184) and bis-acylphosphineoxide, which is now available as Irgacure 1800 from Ciba-Geigy Corporation. Pigmented formulations with varying amounts of pigments between 5 and 20 wt.% are applied electrostatically to medium density fiber board at a layer thickness of 100 microns. Yet, although sufficient hiding is achieved with pigment loadings at 15 wt.% and 20 wt.% pigment, the pendulum hardness and, consequently, the through cure is not fully developed shortly after UV curing, which is undesirable.

The state of the powder coating art, therefore, is that opaquely pigmented or thick filmed UV curable powder coatings cannot be fully cured with UV light.

U.S. Pat. 4,753,817 to Meixner et al. discloses opaquely pigmented liquid UV radiation curable coatings for application to wood, wood-like materials and films of plastic. Such pigmented liquid UV paints are made by incorporating hydroperoxide thermal initiators alongside the UV photoinitiators in liquid resins derived from copolymerizable monomer-free air-drying unsaturated polyesters. The inclusion of the hydroperoxides in the liquid UV formulation is said to improve the cure at the lower layers of the coating that can not be penetrated by UV radiation due to the opacity of the pigments. The liquid paints also contain other essential ingredients not found in powder coatings, including plasticized colloidal cotton, *e.g.*, nitrocellulose, siccatives to promote air-drying, and also volatile organic solvents to adjust the processing viscosity for liquid applications, *e.g.*, toluene, xylene, isopropanol, and butyl acetate. These pigmented UV liquids are first applied to the substrate in liquid form, next pregelled at temperatures of 120°F to 175°F, and then hardened under UV radiation. There is nothing in Meixner et al. that provides any indication that solid compositions could be made that are suitable as powder coatings.

In addition, the liquid UV coatings of Meixner et al. have a number of other shortcomings. For example, the UV liquids contain organic solvents, which generate physiologically and environmentally harmful solvent emissions during drying. As previously mentioned, powder coatings are essentially solventless and nonpolluting substances. The UV liquids also have pot lives only up to 5 hours, which is rather short. This would not be a suitable system for a powder coating which must not advance for several weeks at room temperature, especially in a reclaim powder coating booth. Also, cure for the Meixner et al. system occurs between 120 and 175°F. At such temperatures, significant pregelation or even curing during extrusion would result with a powder coating, which, in turn, would cause processing difficulties as the powder would take a set in the extruder, leading to excessive extruder downtime and expensive clean out costs.

The UV liquids are based on lower molecular weight polyester resins, which are highly reactive liquids at room temperature that cure without crosslinkers. Typical polyester powder coatings require resins with higher molecular weights or higher  $T_g$ 's for the material to remain solid at room temperature, which tends to reduce the reactivity of the resin and require a crosslinker. Also, the UV liquids containing lower molecular weight species would be expected to transport more readily into biological tissues. If improperly handled, the highly reactive UV liquids could be transported through the skin of an individual and poisonously affect physiological functions. The use higher molecular weights species in powder coatings reduces handling problems and reduces the risk of invasion into biological tissues.

Moreover, the liquid UV coatings of Meixner et al. do not require an initial melt and flow out step in order to form a smooth film over the substrate, as required with UV powders, since these coatings are liquids at room temperature and inherently flow out as smooth films when poured. Therefore, incorporation of a thermally activated peroxide cure component in a liquid UV coating is not problematic from a film quality standpoint. However, the inclusion of a thermal peroxide cure component in a UV powder coating would be expected to produce coatings having poor flow out behavior and, consequently, poor film qualities. Conventional wisdom would lead one to expect that the addition of a thermal cure component to a UV curable powder would cause pregelation during the heated flow out step and cause undesirable surface roughness, such as orange peel or low gloss, in the hardened film finish, detrimentally affecting the film quality and aesthetic appearance of the coating. Blisters, craters, pinholes, and other surface defects would also be expected to be visually evident on the surface of the hardened film. Additionally, significant pregelation in the extruder during melt blending the powder ingredients would be expected when using a thermal initiator, causing processing difficulties as the powder blend would begin to cure and take a set in the extruder, which would lead to considerable extruder down time and increased clean out costs.

What is needed is an opaquely pigmented and/or thick filmed UV curable powder coating composition that is suitable for coating heat sensitive substrates, especially wood, wood composites, and plastic, and that can be fully cured through the incorporation of a thermal initiator alongside the usual UV initiator without detracting from the exceptional smoothness of the hardened film finish.

### **Summary of the Invention**

It is an object of this invention, therefore, to provide an opaquely pigmented or thick filmed powder coatings that can be fully cured upon exposure to UV radiation despite the presence of opaque pigments and/or thick films, both of which normally inhibit cure in the coating, through the incorporation of a "dual" cure system, *i.e.*, combination thermal initiator and UV photoinitiator, in the powders, wherein the UV initiator cures the surface, while the thermal initiator cures the lower layers near the substrate, yet without detracting from the exceptional smoothness of the hardened film finish obtained on the surface.

It is another object of this invention to provide dual thermal and UV curable powder coatings that have exceptional smoothness comparable to traditional UV powder coatings.

It is still another object of this invention to provide dual thermal and UV curable powder coatings that have improved through cure properties, including improved adhesion to the substrate, compared to traditional UV curable powder coatings.

It is yet another object of this invention to provide dual thermal and UV curable powder coatings that have relatively low cure temperatures and/or rapid cure speeds for safe curing on heat sensitive substrates without damaging or worsening the substrate.

The present inventors have discovered that the use of dual cure initiators, *i.e.*, a UV initiator along side a thermal initiator, in the powder coatings will give not only excellent surface cure to the film finish, but also superior through cure in the film down to the underlying substrate, while still obtaining exceptional smoothness and desired glossiness in the surface finish. It is quite surprising that the cured powder coating of this invention remains so smooth. Conventional wisdom would lead one to expect that the addition of a thermal cure component to UV curable powders would cause pregelation during the melt and flow out step and, in turn, cause roughness on the surface, such as orange peel or low gloss. Surprisingly, the hardened film finishes produced from powder coatings of this invention are at least as exceptionally smooth as those produced from traditional UV curable powders, while also being fully cured throughout.

The invention resides in a dual thermal and ultraviolet curable powder coating composition, which is a composition in solid particulate form that is a blend of: a) an unsaturated resin selected from unsaturated polyesters, unsaturated polyacrylates, unsaturated polymethacrylates, and mixtures thereof; b) optional second co-polymerizable resin crosslinker having a functional group selected from vinyl ether, acrylate, methacrylate, and allyl ester groups, and mixtures thereof; c) a photoinitiator selected from photolytically activated free radical generating compounds; d) a thermal initiator selected from thermally activated free radical generating compound, such as peroxides, azo compounds, and mixtures thereof; e) an opacifier selected from pigments, fillers, and mixtures thereof; and, f) optional catalyst, wherein the composition can be fully cured, both on the surface and throughout, on a heat sensitive substrate upon exposure of sufficient heat to melt and flow out the powder into a smooth molten film and to activate the thermal

component of the cure, followed by exposure of the molten film to sufficient UV radiation to activate the ultraviolet component of the cure and to form a fully cured smooth hardened film.

The various objects, features and advantages of this invention will become more apparent from the following description and appended claims.

## Detailed Description of the Preferred Embodiments of the Invention

Throughout this specification, all parts and percentages specified herein are by weight unless otherwise stated.

### **Base Resins**

The dual, thermal and UV, curable powder coatings of this invention are primarily based on unsaturated film-forming polymer resins, such as unsaturated polyester resins, unsaturated polyacrylate or polymethacrylate resins, and/or mixtures thereof.

The unsaturated polyester resins useful herein are ethylenically unsaturated condensation reaction products of one or more aliphatic or cycloaliphatic di- or polyfunctional alcohols, or mixtures thereof, and one or more aliphatic, cycloaliphatic, or aromatic di- or polyfunctional carboxylic acids, or mixtures thereof. The carboxylic acids can also be used in their corresponding anhydride form. Corresponding lower alkanol esters are also useful for esterification. Small amounts of monofunctional alcohols and monofunctional carboxylic acids or esters thereof may be present for polyester chain termination purposes. Although unsaturation may be supplied by the alcohol, typically the acid is unsaturated and the alcohol is saturated. Saturated acids can also be present to reduce the density of ethylenic unsaturation in the polyester.

Examples of suitable unsaturated di- and polyfunctional carboxylic acids that are useful herein include maleic anhydride, fumaric acid, citraconic anhydride, itaconic acid, endo-cis-bicyclo[2,2,1]-5-heptene-2,3-dicarboxylic acid, 1,4,5,6,7,7-hexachlorobicyclo[2,2,1]-5-heptene-2,3-dicarboxylic acid (chlorenedic acid), mesaconic acid, dimeric methacrylic acid, and methylbicyclo[2,2,1]-heptene-2,3-dicarboxylic acid. Maleic anhydride, fumaric acid or mixtures thereof are most preferred. It should be understood that whether acids, anhydrides, or lower alkanol esters are listed here, any of these forms are contemplated for use herein.

Examples of suitable saturated diacids or polyacids that are useful herein in combination with a substantial proportion of an unsaturated diacid, include tetrachlorophthalic acid, tetrabromophthalic acid, phthalic anhydride, adipic acid, tetrahydrophthalic acid, isophthalic acid, terephthalic acid, trimellitic acid, azelaic acid, sebacic acid, dimethyl-terephthalate, dimethylisophthalate, succinic acid, dodecanedicarboxylic acid, hexahydrophthalic acid, hexachlorooctahydromethanonaphthalene dicarboxylic acid, malonic acid, glutaric acid, oxalic acid, pimelic acid, suberic acid, and pyromellitic anhydride.

Examples of suitable monoacids that can be used herein to terminate the polyester chain, include linoleic acid, linolenic acid, geranic acid, dehydrogeranic acid, sorbic acid, heptatri-1,3,5-ene-1-carboxylic acid, nonatetra-1,3,5,7-ene-1-carboxylic acid, other fatty acids of vegetable oils, abietic acid, methacrylic acid, and, benzoic acid.

Examples of suitable diols useful herein include ethylene glycol, diethylene glycol, triethylene glycol, 1,2-propylene glycol, 1,3-propylene glycol, 1,4-dimethoxy cyclohexane, 1,2-butylene glycol, 1,3-butylene glycol, 1,4-butylene glycol, 1,2-cyclopentanediol, 1,3-cyclopentanediol, 1,4-cyclopentanediol, 1,2-cyclohexanediol, 1,3-cyclohexanediol, 1,4-cyclohexanediol, 1,4-cyclohexanedimethanol, 4,4'-methylene-bis(cyclohexanol), 4,4'-isopropylidene-bis(cyclohexanol), 1,3-bis(hydroxymethyl)cyclohexane, 1,3-bis(hydroxyethyl) cyclohexane, 1,3-bis(hydroxypropyl) cyclohexane, 1,3-bis(hydroxyisopropyl) cyclohexane, xylene glycol, bisphenol A, hydrogenated bisphenol A, bisphenol A/propylene oxide adducts, hydroquinone/propylene oxide adducts, hydroquinone/ethylene oxide adducts, neopentyl glycol, 1,6-hexanediol, 2,2,4-trimethyl-1,3-pentanediol, 1,3-isobutanediol, 1,2-isobutanediol, 2,3-butanediol, and 2-butenediol(1,4).

Examples of polyols having 3 or more hydroxyl functional groups that are useful herein in small amounts to form branched polyesters, include glycerol, trimethylolpropane, pentaerythritol, allyl ether polyols, polyalkylene glycol ethers, 1,1,1-trimethylol ethane, sorbitol, mannitol, diglycerol, and dipentaerythritol.

Instead of or in addition to the alcohol, epoxy compounds, such as ethylene oxide and propylene oxide, can be used.

Preparation of the unsaturated polyester can be carried out with standard techniques well known in the art. For instance, a two step process may be employed. In the first step, saturated or unsaturated glycols and acids are heated in the presence of an esterification catalyst, such as a tin catalyst, e.g., monobutyl tin oxide, stannous octoate, and monobutyl tin dilaurate, or acid catalyst, e.g., p-toluene sulfonic acid, methane sulfonic acid, and sulfuric acid, at about 400°F to 480°F for about 2 to 24 hours under nitrogen sparge and reacted to a given acid number or hydroxyl number while collecting water formed by esterification. The resultant esterified prepolymer is cooled to about 320°F to 390°F. Glycol loss is measured by refractive index and the lost glycol is added, if needed. Then, in the second step, unsaturated or saturated glycols and acids are charged to the reaction vessel again under nitrogen sparge. The reaction mixture is heated to about 350°F to 450°F for about 2 to 8 hours and reacted to a given acid number, viscosity and amount of

water, if appropriate. The resultant resin is then inhibited with hydroquinone or other substituted phenolic derivative inhibitor.

Unsaturated polyesters resins can also be prepared in a single step by heating saturated and unsaturated polycarboxylic acids with polyols and esterification catalyst, such as stannous oxide, under nitrogen sparge to about 320°F to 480°F for about 1 to 24 hours. The water of esterification is collected to measure the reaction. The glycol loss is again measured and glycol is added, if needed. The reaction is run to the appropriate acid or hydroxyl number and viscosity.

The unsaturated polyester resins can be crystalline, (semi)crystalline, or amorphous. Crystalline and (semi)crystalline unsaturated polyesters are generally preferred over amorphous unsaturated polyesters, since stable powder coatings with lower melt viscosity and better flow can be prepared more easily therefrom.

It is known in the art that certain monomers used in the polycondensation reactions impart crystallinity to the unsaturated polyesters. For example, dihydric alcohol monomers that are known to promote crystallinity include ethylene glycol, 1,4-butanediol, neopentyl glycol, and cyclohexanedimethanol. Dicarboxylic acid monomers that are known to promote crystallization include terephthalic acid and cyclohexane dicarboxylic acid.

The preferred unsaturated polyesters useful herein have a long shelf life without cold flow at temperatures substantially above room temperature up to about 120°F and have a glass transition temperature ( $T_g$ ) or melt temperature ( $T_m$ ) below the desired flow temperature required for preservation of heat sensitive substrates, preferably between about 160°F and about 250°F.

The preferred unsaturated polyesters have a molecular weight ranging between about 400 and about 10,000, more typically about 800 and about 6,800, and, preferably, between about 2,000 and about 4,500.

The unsaturated polyesters preferably have a degree of unsaturation between about 2 and about 20 wt. % unsaturation, and, preferably, between about 4 and about 10 wt. % unsaturation.

Whether the polyester is carboxylic acid-functionalized or hydroxyl-functionalized depends upon the -COOH/-OH molar ratio of the monomer mix. If the unsaturated polyester is hydroxyl-functionalized, then the hydroxyl number of the polyester is generally between about 5 and about 100, and, preferably, between about 9 and about 50. If the unsaturated polyester is acid-functionalized, then the acid number of the polyester is generally between about 1 and about 80, and, preferably, between about 9 and about 50.

Preferably, the unsaturated polyesters are solid resins at room temperature or above, so that they can be easily formulated into nonsintering powders. If the resins are liquids, they should be converted to powder form and, thus, be counted as a solid by absorption onto inert silica-type filler materials, such as fumed silica, before use, as is well known in the art.

Exemplary unsaturated polyester formulations useful herein are further specified in the working examples.

The unsaturated acrylate and methacrylate resins useful herein include polymers containing unreacted acrylate or methacrylate groups in the main chain or side chain. The unsaturated acrylate or methacrylate polymers are the reaction products of one or more solid functional polymers having reactive functional groups with one or more copolymerizable monomers having co-reactive functional groups capable of reacting with the functional groups of the polymer, with at least one of the functional polymer or copolymerizable monomer also containing an acrylate or methacrylate group available for final curing of the resin. The unsaturated acrylate or methacrylate polymer obtained in the aforesaid reaction may be an acrylated epoxy, acrylated urethane, acrylated polyether, or acrylated polyester resin, or their corresponding methacrylates.

The polymers containing unreacted acrylate or methacrylate groups in the side chains can be prepared by standard techniques well known in the art. For instance, a two step process may be employed. In the first step, a solid functional polymer is formed using standard polymerization techniques. For example, the polymer formed in step one can be a functionalized acrylate or methacrylate polymer.

Suitable monomers which are commonly used to form the backbone of such functionalized acrylate and methacrylate polymers, include methyl acrylate, methyl methacrylate, ethyl acrylate, ethyl methacrylate, n-butyl acrylate, n-butyl methacrylate, isobutyl acrylate, isobutyl methacrylate, 2-ethylhexyl acrylate, 2-ethylhexyl methacrylate, and the like. In addition, suitable amounts of functional monomers are copolymerized during polymerization to obtain the functionalized polymer. Acid-functional acrylate or methacrylate polymers can be formed from acid-functional monomers, such as acrylic acid and methacrylic acid. Hydroxyl-functional acrylate or methacrylate polymers can be formed from hydroxyl-functional monomers, such as 2-hydroxyethyl methacrylate, 2-hydroxypropyl methacrylate, 3-hydroxypropyl methacrylate, 3,4-dihydroxybutyl methacrylate. Epoxy-functional acrylate or methacrylate polymers can be formed from epoxy-functional monomers, such as glycidyl methacrylate, 2,3-epoxybutyl methacrylate, 3,4-epoxybutyl methacrylate, 2,3-epoxycyclohexyl methacrylate, and 10,11-epoxyundecyl methacrylate. Isocyanate-functional polymers can also be formed from isocyanate functional monomers, such as meta-isopropenyl-a,a-dimethylbenzylisocyanate (TMI).

The functional polymers formed in step one that will be reacted with bi-functional acrylate or methacrylate monomers can also be other types of solid resins, other than acrylates or methacrylates, having acid, hydroxyl, epoxy or

isocyanate functional groups, for example, epoxidized bisphenol A resins or acid, hydroxyl, or isocyanate functionalized polyester resins.

In the second step, a reaction is carried out between the unreacted functional groups of the solid functional polymer formed in step one with a co-polymerizable monomer having both a co-reactive functional group capable of reacting with the reactive functional groups of the functional polymer and an unsaturated acrylate or methacrylate group available for final curing of the resin. Any one of the functionalized acrylate or methacrylate monomers listed above can serve as this bi-functional co-polymerizable monomer.

The reaction is carried out by dissolving the above formed solid functional polymer in an appropriate solvent for the polymer, such as butyl acetate, and then adding the bi-functional co-polymerizable monomer having pendent acrylate or methacrylate unsaturated groups in a stepwise manner at elevated temperatures between, for example about 150°F and 300°F, until substantial completion of the reaction. This reaction can also be done without solvent by heating the reactants above their melting points. For example, in the second step an acid-functional acrylate or methacrylate polymer can be reacted with a compound having an epoxy group, such as an epoxy-containing acrylate or methacrylate monomer, *e.g.*, glycidyl methacrylate, to form a methacrylated polyester. An isocyanate-functional polymer, *e.g.*, TMI, can likewise be reacted with a hydroxy-functional acrylate or methacrylate monomer, such as 2-hydroxyethyl methacrylate, to form an acrylated urethane.

Resins containing acrylate or methacrylate groups in the main chain can be prepared by reacting epoxy-, carboxyl-, hydroxyl-, or isocyanate-containing resins with bi-functional acrylate or methacrylate monomers having functional groups co-reactive with the aforesaid functionalities. For example, an epoxy-functional polymer, such as polyglycidyl methacrylate or epoxidized bisphenol A resin, can be reacted with a monomer having acid group, such as acrylic acid or methacrylic acid. In this reaction, the heat must be closely monitored to assure that the acrylic acid does not polymerize. In addition, an acid-functional polyester, such as one prepared from neopentyl glycol, ethylene glycol, adipic acid and isophthalic acid, can be reacted with a bi-functional acrylate or methacrylate compound having epoxy groups, such as glycidyl methacrylate. Also of note is the reaction of acrylic or methacrylic acid with an alcohol or hydroxyl functional polyester at elevated temperatures to form a polyester with acrylate functionality.

The unsaturated group left in the polymer for final curing of the powder coating need not be an acrylate or methacrylate group, although an unsaturated acrylate or methacrylate unsaturation is most preferred. It is also possible to form other solid resins having allyl, vinyl, vinyl ether, and styryl functionalities. For example, a hydroxyl functional polyester resin, such as one made with neopentyl glycol, 1,4-cyclohexene dimethanol, terephthalic acid and adipic acid, can be reacted with TMI, to form a styryl-functional resin.

The unsaturated acrylated or methacrylated polymer would be used similarly to the unsaturated polyester resin in this portion of the formulation. The  $T_g$ , molecular weight, and % unsaturation range would be similar to that used for the unsaturated polyesters. The % unsaturation in this case will be governed by the amount of acrylate or methacrylate in the polymer. Whereas the % unsaturation in the polyester is governed by the maleic or fumaric content of polyester.

The acrylate or methacrylate polymer resins are capable of crosslinking without an additional crosslinking agent, although crosslinkers may be used with such formulations.

Preferably, the unsaturated polyacrylate and polymethacrylate resins are solids at room temperature or above, so that they can be easily formulated into nonsintering powders. If the resins are liquids, they should be converted to powder form and, thus, be counted as a solid, by absorption onto inert silica-type filler materials, such as fumed silica, before use, as is well known in the art.

Exemplary unsaturated acrylate or methacrylate polymer formulations useful herein are further specified in the working examples.

### Crosslinkers

The unsaturated polyester resins useful herein work best in combination with co-polymerizable second resins having ethylenic unsaturation and preferably having two sites of unsaturation per molecule. These second resins are used in the composition as crosslinkers for the base resin. Most preferred is a predominance of monomers or prepolymers that are solid at room temperature or above, so that they can be easily formulated into nonsintering powders.

The co-polymerizable second resins or crosslinkers useful herein are preferably oligomers or polymers having vinyl ether, acrylate or methacrylate, or allyl ester groups, with an oligomer or polymer having vinyl ether groups being most preferred.

The co-polymerizable second resins having vinyl ether groups are preferably composed of vinyl ether functionalized urethanes, for example, a divinyl ether urethane based on the reaction product of a diisocyanate, such as hexamethylene diisocyanate, and a hydroxyl-functional vinyl ether, such as hydroxybutyl vinyl ether. Other suitable hydroxyl-functional vinyl ethers include hydroxyethyl vinyl ether and trimethylene glycol monovinyl ether. Other suitable diisocyanates include isophorone diisocyanate, methylene diisocyanate, methylenebiscyclohexylisocyanate, trimethylhexamethylene diisocyanate, hexane diisocyanate, hexamethyl diisocyanate, hexamethylamine diisocyanate, methyl-

enebiscyclohexyl isocyanate, toluene diisocyanate, 1,2-diphenylethane diisocyanate, 1,3-diphenylpropane diisocyanate, diphenylmethane diisocyanate, dicyclohexylmethyl diisocyanate, and other isocyanate prepolymers and terpolymers. Functional prepolymers derived from these diisocyanates, such as urethane trimers, uretdiones, isocyanurates, and biurets can also be used.

The functionalized vinyl ethers can be obtained in a conventional manner. For example, vinyl ether urethanes are usually prepared by reacting a hydroxyl-functional vinyl ether with a multi-functional isocyanate-containing monomer or polymer in solvent, such as methylene chloride, under a nitrogen atmosphere, at temperatures between about ambient and 125°C. Additional reference can be made to U.S. Pat. 4,751,273 to Lapin et al. for the preparation of vinyl ether functionalized urethanes, which disclosure is incorporated by reference herein in its entirety. Examples of vinyl ether urethanes are sold under the trade names Uralac resins by DSM Resins and Vectomer Oligomers and Diluents by Allied Signal.

Preferably, vinyl ether urethane prepolymers that are non-crystalline solids at room temperature or higher are used so that they can easily be formulated into non-sintering powders. These non-crystalline solid materials can be obtained by reacting a non-crystallizing diisocyanate monomer, such as isophorone diisocyanate with a crystallizing or non-crystallizing polyol, such as neopentyl glycol, and then reacting the isocyanate urethane adduct obtained with a hydroxy vinyl ether, such as 4-hydroxybutyl vinyl ether, or otherwise by reacting a non-crystallizing aliphatic polyisocyanate, such as isophorone diisocyanate trimer, with a hydroxy vinyl ether, such as 4-hydroxybutyl vinyl ether. The reactions are typically carried under a nitrogen atmosphere, in the presence of tin catalyst, such as dibutyltin dilaurate, at temperatures not above about 100-110°C. Due to the polymeric nature of the so prepared vinyl ether urethanes, powder coatings based on the same exhibit improved flexibility and adhesion to the substrate after curing. Also, such higher molecular weight materials are relatively safer to handle and have lower toxicities than traditional vinyl ether urethane curing agents. For a further description of such non-crystalline solid vinyl ether curing agents, reference can be made to the U.S. Patent Application of Navin B. Shah and Andrew T. Daly entitled *Solid Vinyl Ether Terminated Urethane Curing Agent*, filed this same day, which disclosure is incorporated by reference herein in its entirety.

The co-polymerizable second resins having acrylate or methacrylate groups are preferably composed of dimethacrylate functionalized urethanes, for example, based on diisocyanate, such as hexanediisocyanate, and a hydroxyl-functional methacrylate, such as hydroxyethyl methacrylate. Other isocyanates can be used as well such as those listed above. In addition, other suitable hydroxyl-functional methacrylates include hydroxypropyl methacrylate and other hydroxy alkyl methacrylates. This material can be reacted the same as the vinyl ethers above.

The co-polymerizable second resins having allyl ester groups are preferably composed of hydroxy functional allyl esters, for example, based on the esterification reaction product of allyl alcohol and phthalic anhydride, which forms diallyl phthalate. Examples of suitable allyl functionalized oligomers, include diallyl phthalate prepolymers, iso-diallyl phthalate prepolymers, p-diallyl phthalate prepolymers, diallyl maleate, triallyl cyanurate, diallyl chlorendate methacrylamide, and triallylisocyanurate.

If the co-polymerizable second resin is a liquid or a sticky powder and is used in sufficient quantities that the resultant melt blended powder coating composition is not adequately free flowing, then this coreactant can be absorbed on an inert filler, such as fumed silica, and thus be counted as a solid within the preferred scope of this invention. Except in small quantities up to about 5 wt. % of the powder coating composition, these liquids species are much less preferred than solid co-reactants due to sintering problems.

The relative amounts of unsaturated polymer base resin to unsaturated copolymerizable second resin provided in the powder coating compositions of this invention depend in part on the choice of materials. For instance, when the resin is an unsaturated polyester and the second resin crosslinker is a vinyl ether functionalized compound, the equivalent ratio of polyester unsaturation to vinyl ether unsaturation is between about 90:10 and about 10:90, and, preferably about 50:50. When the resin is an unsaturated polyester and the second resin crosslinker is an allyl ester functionalized compound, the equivalent ratio of polyester unsaturation to allyl ester unsaturation is between about 99:1 and about 1:99, and, preferably, between about 70:30 and about 95:5. When the resin is a acrylate or methacrylate polymer, it is preferred to not use a crosslinker.

Exemplary crosslinker formulations useful herein are further specified in the working examples.

## UV Photoinitiators

UV photoinitiators that are incorporated in the powder coating compositions to impart a radiation activated, rapid, and low temperature cure to the powder are well known in the art. Examples of suitable photoinitiators, which are known as alpha cleavage free radical photoinitiators, include benzoin and its derivatives, for example, benzoin ethers, such as isobutyl benzoin ether and benzyl ketals, such as benzyl dimethyl ketal, 2-hydroxy-2-methyl-1-phenylpropan-1-one and 4-(2-hydroxyethoxy) phenyl-2-hydroxy-2-propyl ketone. Others include acyl phosphines, such as 2,4,6-trimethylbenzoyl diphenylphosphine oxide. Aryl ketones can also be used, such as 1-hydroxycyclohexyl phenyl ketone, 2-benzyl-2-dimethylamino-1-(4-morpholinophenyl)-butan-1-one, 2,2-dimethoxy-2-phenylaceto-phenone, mixture of



benzophenone and 1-hydroxycyclohexyl phenyl ketone, perfluorinated diphenyl titanocene, and 2-methyl-1-(4-(meth-  
ylthiophenyl)-2-(4-morpholinyl))-1-propanone.

Hydrogen abstraction free radical type photoinitiators can be used in combination with the above or alone such  
as Michler's ketone (4,4'-bisdimethylamino benzophenone), Michler's ethyl ketone (4,4'-bisdiethylamino benzophe-  
none ethyl ketone), benzophenone, thioxanthone, anthroquinone, d,l-camphorquinone, ethyl d,l-camphorquinone, ke-  
tocoumarin, anthracene, or derivatives thereof, and the like.

Cationic polymerization, especially with vinyl ether containing crosslinkers, can proceed via cationic cure using  
cationic photoinitiators. Major classes of cationic photoinitiators are diaryliodonium salts and copper synergists, such  
as diphenyl iodonium hexafluorophosphate, dibenzyl iodonium hexafluoroarsinate and copper acetate, triarylsulfonium  
salts, such as triphenyl sulphonium hexafluorophosphate, triphenyl sulphonium tertafluoroborate. Dialkylphenacyl- sul-  
fonium salts, ferrocenium salts, such as cyclopentadienyl iron(II) hexafluorophosphate, alpha-sulfonyloxy ketone, and  
silyl benzyl ethers can be used as well.

Preferably, the photoinitiators used herein are solids. If liquid initiators are used, however, preferably they are  
absorbed on solid carriers, such as fumed silica, prior to incorporation in the powder coating compositions of this  
invention.

In general, the amount of photoinitiator used in the powder coating composition of the present invention ranges  
between about 0.1 and 10 parts per hundred resin (phr), and preferably between about 1 and 5 phr.

Exemplary photoinitiator formulations useful herein are further specified in the working example.

Reference can also be made to EP 0 636 669 A2 to DSM, N.V. for further examples of the aforementioned base  
resins, crosslinkers, and photoinitiators, which disclosure is incorporated by reference herein in its entirety.

### Thermal Initiators

The thermal initiators useful in the powder coating compositions of this invention are free radical generating com-  
pounds, preferably peroxides and azo initiators. Examples of suitable peroxide initiators, include diacyl peroxides, such  
as 2-4-dichlorobenzyl peroxide, diisononanoyl peroxide, decanoyl peroxide, lauroyl peroxide, succinic acid peroxide,  
acetyl peroxide, benzoyl peroxide, and diisobutyl peroxide, acetyl alkylsulfonyl peroxides, such as acetyl cyclohex-  
ylsulfonyl peroxide, dialkyl peroxydicarbonates, such as di(n-propyl)peroxy dicarbonate, di(sec-butyl)peroxy dicarbo-  
nate, di(2-ethylhexyl)peroxy dicarbonate, diisopropylperoxy dicarbonate, and dicyclohexylperoxy dicarbonate, peroxy  
esters, such as alpha-cumylperoxy neodecanoate, alpha-cumylperoxy pivalate, t-amyl neodecanoate, t-amylperoxy  
neodecanoate, t-butylperoxy neodecanoate, t-amylperoxy pivalate, t-butylperoxy pivalate, 2,5-dimethyl-2,5-di(2-ethyl-  
hexanoylperoxy)hexane, t-amylperoxy-2-ethyl hexanoate, t-butylperoxy-2-ethyl hexanoate, and t-butylperoxy isobu-  
tyrate, azobis (alkyl nitrile) peroxy compounds, such as 2,2'-azobis-(2,4-dimethylvaleronitrile), azobisisobutyronitrile,  
and 2,2'-azobis-(2-methylbutyronitrile); t-butyl-peroxymaleic acid, 1,1'-azobis-(1-cyclohexanecarbonitrile).

Other thermal initiators, include peroxy ketals, such as 1,1-di(t-butylperoxy)-3,3,5-trimethylcyclohexane, peroxy  
esters, such as o,o'-t-butyl-o-isopropyl monoperoxy carbonate, 2,5-dimethyl-2,5-di(benzoylperoxy) carbonate, o,o'-t-  
butyl-o-(2-ethylhexyl)-monoperoxy carbonate, t-butylperoxy acetate, t-butylperoxy benzoate, di-t-butyl diperoxy aze-  
late, and di-t-butyl diperoxy phthalate, dialkylperoxides, such as dicumyl peroxide, 2,5-dimethyl-2,5-di(t-butylperoxy)  
hexane, t-butyl cumyl peroxide, di-t-butyl peroxide, and 2,5-dimethyl-2,5-di(t-butylperoxy)hexyne-3, hydroperoxides,  
such as 2,5-dihydroperoxy-2,5-dimethyl hexane, cumene hydroperoxide, t-butyl hydroperoxide and t-amyl hydroper-  
oxide, ketone peroxides, such as n-butyl-4,4-bis-(t-butylperoxy)valerate, 1,1-di(t-butylperoxy)-3,3,5-trimethyl cyclohex-  
ane, 1,1'-di-t-amyl-peroxy cyclohexane, 2,2-di(t-butylperoxy) butane, ethyl-3,3-di(t-butylperoxy)butyrate, and blend of  
t-butyl peroctoate, and 1,1-di(t-butylperoxy)cyclohexane.

Also included are o,o'-t-alkyl-o-alkylmonoperoxy carbonates, such as o,o'-t-butyl-o-isopropylmonoperoxy carbon-  
ate, p,p'-oxybis(benzene sulfonyl) hydrazide, and accelerated azocarbonamide.

Preferably, the thermal initiators used herein are solids. If liquid initiators are used, however, preferably they are  
absorbed on solid carriers, such as fumed silica, prior to incorporation in the powder coating compositions of this  
invention.

In general, the amount of thermal initiator used in the powder coating composition of the present invention ranges  
between about 0.1 and about 10 phr, and, preferably, between about 1 and about 6 phr.

Exemplary thermal initiator formulations useful herein are further specified in the working examples.

### Catalysts

It sometimes may be desirable to include a catalyst in the powder coatings to increase rate of crosslinking. As  
catalysts, metal compounds based on a fatty acid or oil may incorporated in the powders. Examples of suitable metals  
are cobalt, manganese, lead, copper, and vanadium. Cobalt-containing compounds, especially cobalt acids, for exam-  
ple, cobalt octoate, cobalt neodecanoate, cobalt naphthenate, and cobalt octadecanoate, are preferred. The metal-

containing compounds provide improved cure, especially in thermal peroxide initiated cure systems. Through a redox process, the metal catalysts tend to decompose hydroperoxides created by oxygen inhibition near the coating surface. Amines, such as, for example, dimethylaniline, may also be used as the catalyst.

Such compounds, if used, are preferably employed in amounts of less than about 1.0 phr, and typically in the range between about 0.1 and about 0.5 phr.

### Opacifiers

The powder coating compositions of this invention can be opacified or pigmented without diminishing the through cure properties. Examples of suitable pigments useful herein, include carbon black, Shepard black No. 1, titanium dioxide white, chromium oxide green, zinc oxide, iron oxide yellows, reds, browns and blacks, such as ferrite yellow oxide, ferric oxides, raw sienna and burnt sienna, lead chromate, copper phthalonitrile blue, phthalocyanine blues and greens, ultramarine blue, toluidine red, parachlor red, cadmium reds and yellows, phthaloorganamine blues and greens, iron blues, organic maroons, and the like. Especially useful are lower reflecting pigments such as anatase titanium dioxide, zinc sulfide, and the mixed metal oxide pigments, such as manganese ferrite black, chromium green black hematite, cobalt aluminate blue spinel, copper chromite black spinel, and sodium alumina sulfosilicate. Also possible with this technology are metallics made with aluminum, mica, or brass.

Fillers may also be used to opacify or lower the gloss of the powder coating without diminishing the through cure properties. Examples of suitable fillers useful herein, include silica, such as fumed silica, glass frit, flour, calcium carbonate, barium sulfate, mica, ammonium chloride, ammonium bromide, boric acid, antimony trioxide, fumed alumina, clays such as kaolin, china clay, talc, lithopone, zinc sulfide, lead titanate, zirconium oxide, white lead, barium oxide, calcium oxide or hydroxide, magnesium oxide or hydroxide, chalk, asbestos, ceramic, hollow glass, resin microspheres, pearl essence, barytes, diatomaceous earth, aluminum trihydrate, onyx flour, calcium silicate, mixed silicates, and the like.

In general, the amount of pigments, fillers and opacifiers used in the powder coating composition of the present invention ranges between about 0.1 and about 100 phr, and, preferably, between about 1 and 60 phr. However, loadings can vary depending on the desired opacity of the dry film.

### Other Ingredients

In addition to the aforementioned components, the powder coating composition of this invention may also contain conventional powder coating additives, such as gloss control aids, powder flow aids, leveling agents, dispersants, anticratering agents, stabilizers and other standard materials.

Gloss control agents such as polyethylene waxes, oxidized polyethylenes, polyamides, teflons, polyamides may be used in a formulation to adjust or obtain a lower gloss coating.

Preferred powder flow aids that may be employed in the powder coating of this invention are acrylic or silicone flow aids, which are composed of acrylic or silicone resins, respectively. The acrylic resins are generally liquids which have been converted to powder form by absorption onto silica-type materials. An example of an acrylic flow aid is sold under the trade name Resiflow P67 by Estron Chemical, which is a 2-propenoic acid, ethyl ester polymer. Examples of other suitable acrylic flow aids are acrylic resins sold under the trade name BYK 352 and BYK 300 by BYK Chemie. When used, the powder flow aid is generally provided in an amount between about 0.1 and about 6 phr, and, preferably, between about 0.7 and about 1.5 phr, in the thermosetting powder coating compositions of this invention.

Dry flow additives are normally employed, such as fumed silica or alumina oxide, to reduce the tendency to cake or block during transportation or use. An example of a fumed silica is sold under the trade name Cab-O-Sil by Cabot Corporation. An example of an aluminum oxide is sold under the trade name Aluminum Oxide C by Degussa Corporation. When used, the dry flow additive is generally provided in an amount between about 0.05 and about 0.5 phr, and, preferably, between about 0.1 and about 0.3 phr.

Outgassing or anticratering aids can be used in these formulations to reduce or eliminate bubbles or trapped gas from the substrate or coating. Typical outgassing aids include, benzoin (2-hydroxy-1,2-diphenylethanone) and its analogs, and plasticizers, such as low molecular weight phenoxies and phthalates. When used, the outgassing aid is generally provided in an amount between about 0.1 and about 15 phr, and, preferably, between about 1 and about 5 phr.

UV stabilizers are also commonly used to improve weathering, such as UV absorbers and hindered amine- or hindered phenol-like stabilizers. When used, the UV stabilizers are generally provided in an amount between about 0.1 and about 5 phr, and, preferably, between about 1 and about 3 phr.

### Powder Preparation

The powder coatings of this invention are prepared by conventional techniques employed in the powder coatings

art. Typically, the components of the powder coating formulation are thoroughly blended together by medium to high intensity mixing until the mixture is homogeneous and dry, and then melt blended, preferably in an extruder. Any ingredients which are liquid at the mixing temperature can optionally be absorbed onto a dry substrate which may constitute one of the other ingredients of the mixture. Melt blending is generally carried out in the temperature range of between about 160°F and about 300°F, and, preferably, between about 180°F and about 250°F, with careful control of the extruder temperature to minimize any curing and gelation from taking place in the extruder. Extrusion with a supercritical fluid, such as supercritical CO<sub>2</sub>, may be desirable with powders containing crystalline materials. The extruded composition, usually in sheet form after cooling substantially to room temperature, is broken into chips and then ground in a mill to a powder, while carefully controlling the temperature between about -160°F (cryogenic) and about 90°F, and, preferably, between about 0°F and about 75°F, and then subsequently screened to achieve the desired powder particle size, typically having an average particle size of about 30 microns.

The prepared powder coatings of this invention exhibit the following properties: long shelf life at temperatures preferably up to about 90°F; ability to flow out at relatively low temperatures preferably between about 160°F and about 250°F; relatively low flow viscosity; ability to be fully cured throughout, especially at the lower layers near the substrate, despite the presence of opaque pigments or thick films, ability to form exceptionally smooth films having the desired glossiness despite the presence of a thermal initiator; rapid cure; together with desirable other properties, such as good flexibility, adhesion, hardness, scratch resistance, etc.

### Coating Method

First, the powder coatings of this invention are applied in dry, free flowing, solid powder form over the substrate to be coated. Preferably, powders are sprayed onto the substrate by well known electrostatic powder spray techniques, such as corona discharge or triboelectric electrostatic spray techniques.

Next, the powders are exposed to only enough heat to melt, level and flow out the powders into a continuous molten film having the desired smoothness, and activate the thermal component of the cure. Heating may take place in either infrared (IR) or convection ovens, or a combination of both.

The applied powders of this invention become molten at sufficiently low temperatures and form smooth films at very rapid speeds, so as not to cause damage to a heat sensitive substrate. The powder flow temperature is relatively low, preferably between about 160°F and about 250°F, and it preferably takes only between about 5 and about 190 seconds for the powder to adequately flow out as a smooth, continuous, uniform, molten film over the substrate. The flow viscosity is also sufficiently low, for example, between about 100 and 4,000 cone and plate, which allows the powder to have good flow out behavior on heating to result in smooth coatings. Sufficient outgassing of substrate volatiles simultaneously occurs during the flow out step to eliminate surface defects, such as blisters and pin holes. The reduced temperature cure of these powders also helps eliminate outgassing, especially in porous metal substrates, such as cast aluminum and zinc, and also in heat sensitive substrates, such as wood and plastic.

While the powder coatings are molten, the films are exposed to a UV light source, such as medium pressure mercury vapor lamps or gallium lamps, for example, Fusion H-, D-and/or V-lamps, to activate the ultraviolet component of the cure and to rapidly cure the films into smooth hardened finishes. Electron beam radiation can be used as well.

Upon exposure to UV radiation, the molten films are rapidly hardened between about 1 millisecond and about 10 seconds, and, preferably, less than about 3 seconds. The hardened dry film finishes formed on the substrate preferably have a thickness of between about 0.5 and about 25 mils, and, more preferably, between about 1 and about 10 mils. UV hardened thicker films, e.g., more than 2 mils, can be formed with a single coat which has not heretofore been possible.

Thick films and pigmented films can be essentially fully cured as well as thin and clear films using the powder coatings of this invention, resulting from the presence of a thermal initiator in the coating.

Despite the presence of the thermal initiator, the hardened film finishes produced from the powder coatings of this invention surprisingly have substantially the same exceptional smoothness as that of standard UV curable powder coatings. The powder coating film finish gives off the appearance of being a plastic coating or laminate.

The surprising finding is that the thermal initiator, such as a peroxide, improves through cure and adhesion to the substrate without impairing the flow out behavior and without detracting from the smoothness and desired glossiness of the cured film.

The powder coatings of the present invention are found to be particularly useful when applied to heat sensitive substrates, such as wood, wood composites, and plastic, due to the low temperature and rapid cure aspects of these coatings. Using the aforesaid heating and UV curing techniques, it is possible to limit the thermal load on the substrate to acceptable levels for heat sensitive substrates, so as not to cause embrittlement, loss of integrity, deformation, and other damage to the physical and/or chemical properties of the heat sensitive substrates.

However, it should be understood that the invention is not limited to heat sensitive substrates, and the powder coatings of this invention can form the same smooth hardened film finishes on heat resistant substrates, such as metal,

as well. Exemplary substrates that can be coated with the powder coatings of this invention are listed hereinbelow.

### Heat Sensitive Substrates

Examples of suitable heat sensitive substrates useful herein, include wood, such as hardwood, hard board, laminated bamboo, wood composites, such as particle board, electrically conductive particle board, fiber board, medium density fiber board, masonite board, laminated bamboo, and other substrates that contain a significant amount of wood. Any of these wood based substrates may be filled or primed with materials, such as UV liquids, powder primers, or solvent or waterborne coatings to improve smoothness and reduce film builds. The wood substrates are typically used in kitchen cabinetry, shelving and storage units, home and business furniture, computer furniture, etc.

Other heat sensitive substrates are plastics, such as ABS, PPO, SMC, polyolefins, acrylics, nylons and other copolymers which usually will warp or outgas when coated and heated with traditional heat curable powders. The plastics are typically used in automotive parts. Still other heat sensitive substrates include paper, cardboard, and composites and components with a heat sensitive aspect, and the like.

### Heat Resistant Substrates

Examples of suitable heat resistant substrates, include metal, such as steel and other alloys, which are typically used for building panels, rebars, pipelines, cold coil springs, and steel strapping. Other heat resistant substrates, include glass, ceramic for ceramic tiles, carbon and graphite.

The invention will be further clarified by a consideration of the following specific examples which are intended to be purely exemplary of the invention.

### Example 1

#### Preparation of Pigmented Polyester/Vinyl Ether Powder Coating With Dual Thermal and UV Cure

The ingredients listed below in Table 1A were compounded as described to form a pigmented powder coating of this invention having a dual cure, thermal and UV, aspect.

### Comparative Example 1

#### Preparation of Pigmented Polyester/Vinyl Ether Powder Coating With UV Cure Only

The ingredients listed below in Table 1A were compounded as described to form a pigmented powder coating having a UV cure aspect only.

Table 1A

Ingredients	Phr	
	Example 1	Comp. Ex. 1
DRY BLEND UNTIL HOMOGENEOUS		
XP 3125 Unsaturated Polyester <sup>1</sup>	80	80
ZW 3307 Vinyl Ether <sup>2</sup>	20	20
Lucerin TPO Photoinitiator <sup>3</sup>	2	2
Irgacure 184 Photoinitiator <sup>4</sup>	1	1
Resiflow P67 Acrylic Flow Aid <sup>5</sup>	1.5	1.5

<sup>1</sup> XP 3125 Unsaturated Polyester is a solid, acid-functional, semicrystalline polyester resin that is believed to be derived from fumaric acid, terephthalic acid, and 1,6-hexanediol, and that is commercially available from DSM Resins.

<sup>2</sup> ZW 3307 Vinyl Ether is a solid, divinyl ether functionalized urethane crosslinker resin that is believed to be derived from derived from hexamethylene diisocyanate and 4-hydroxybutyl vinyl ether, and that is commercially available from DSM Resins.

<sup>3</sup> Lucerin TPO Photoinitiator is a 2,4,6-trimethylbenzoyldiphenyl phosphine oxide that is commercially available from BASF.

<sup>4</sup> Irgacure 184 Photoinitiator is an aryl ketone, 1-hydroxycyclohexyl phenyl ketone, that is commercially available from Ciba Additives.

<sup>5</sup> Resiflow P67 Acrylic Flow Aid is a polyacrylate, which is a 2-propenoic acid ethyl ester polymer that is commercially available from Estron Chemical.

Table 1A (continued)

Ingredients	Phr	
	Exemple 1	Comp. Ex. 1
DRY BLEND UNTIL HOMOGENEOUS		
Lupersol 230XL Peroxide <sup>6</sup>	2	0
TiPure R-902 Titanium Dioxide <sup>7</sup>	25	25
Total	131.5	129.5
CHARGE TO EXTRUDER AND EXTRUDE TO SHEETS		
MELT TEMPERATURE = 200°F		
AIR COOL AND BREAK INTO CHIPS		
CHARGE TO MILL AND GRIND TO POWDER AT HIGH SPEED		
SCREEN TO -140 MESH		

<sup>6</sup>Lupersol 230XL Peroxide is a peroxy ketal, 1,1bis(t-butylperoxy)3,3,5-trimethylcyclohexane on an inert filler at 40% active ingredient that is commercially available from Elf Atochem.

<sup>7</sup>TiPure R-902 is a white titanium dioxide pigment that is commercially available from Du Pont.

## Results

The powder coating compositions listed in Table 1A were electrostatically sprayed with a tribo gun to about 3 to 6 mils on respective ½" particle boards. The boards were heated with quartz IR lamps for about 30 sec. to about 250°F in order to form a molten film. Next, the boards were immediately conveyed through a UV source and cured by exposure to UV radiation, first with a V-lamp and then with a H-lamp, at about 30 ft./min. for about one second. The cured powder coatings were then subjected to performance tests with the test results listed below in Table 1 B.

Table 1B

Test	Result	
	Example 1	Comp. Ex. 1
Cross Hatch Adhesion	3B/4B	0B/1B
Appearance	Moderate Orange Peel	Moderate Orange Peel
Outgassing	None	Slight
Solvent Resistance (50 Double Rubs)	No Effect	No Effect
Pencil Hardness Mar	3H	F

## Example 2

### Preparation of Pigmented Polyester/Allyl Ester Powder Coating With Dual Thermal and UV Cure

The ingredients listed below in Table 2A were compounded as described to form a pigmented powder coating of this invention having a dual cure, thermal and UV, aspect.

### Comparative Example 2

### Preparation of Pigmented Polyester/Allyl Ester Powder Coating With Peroxide Cure Only

The ingredients listed below in Table 2A were compounded as described to form a pigmented powder coating having a thermal peroxide cure aspect only.

Table 2A

Ingredients	Phr	
	Example 2	Comp. Ex. 2
DRY BLEND UNTIL HOMOGENEOUS		
Pioester 275 Unsaturated Polyester <sup>1</sup>	80	80
Iso Diallyl Phthalate <sup>2</sup>	20	20
Resiflow P67 Acrylic Flow Aid	1.5	1.5
Benzoin <sup>3</sup>	0.8	0.8
Lupersol 231 Peroxide <sup>4</sup>	3	3
Benzyl Dimethyl Ketal Photoinitiator <sup>5</sup>	2	0
TiPure R-902 Titanium Dioxide	20	20
Total	127.3	125.3
CHARGE TO EXTRUDER AND EXTRUDE TO SHEETS		
MELT TEMPERATURE = 180°F		
AIR COOL AND BREAK INTO CHIPS		
CHARGE TO MILL AND GRIND TO POWDER AT HIGH SPEED		
SCREEN TO -140 MESH		

<sup>1</sup>Pioester 275 Unsaturated Polyester is a solid, acid-functional, semicrystalline unsaturated polyester resin that is derived from maleic anhydride with 7% unsaturation and an acid number of 35, and that is commercially available from Pioneer Plastics.

<sup>2</sup>ISO Diallyl Phthalate is an allyl ester functional crosslinking agent that is commercially available from GCA Chemical.

<sup>3</sup>Benzoin is a degassing and anti-cratering agent that is commercially available from Estron Chemicals.

<sup>4</sup>Lupersol 231 Peroxide is a peroxy ketal, 1,1-bis(t-butylperoxy)3,3,5-trimethylcyclohexane, that is commercially available from Elf Atochem.

<sup>5</sup>Benzyl Ketal Dimethyl Ketal Photoinitiator is a benzyl ketal UV initiator that is commercially available from Ciba Additives.

## Results

The powder coating compositions listed in Table 2A were electrostatically sprayed with a tribo gun on respective ½" medium density fiber boards preheated using infrared lamps to about 200°F to 250°F. The boards were post heated with quartz IR lamps for up to 2 minutes at about 300°F for the peroxide sample only in order to melt and cure the powder and for about 30 sec. at about 300°F for the dual cure sample in order to initiate thermal cure and form a molten film. After flow out, the dual cure sample was immediately cured by exposure to UV radiation, first with a V-lamp and then with a H-lamp, at about 30 ft./min. for about one second. The cured powder coatings were subjected to performance tests with the test results listed below in Table 2B.

Table 2B

Test	Result	
	Example 2	Comp. Ex. 2
Cross Hatch Adhesion	5B	5B
Appearance	Moderate Orange Peel	Moderate Orange Peel
MEK Resistance (50 Double Rubs)	5 No Effect	3 Moderate Rub Off
Pencil Hardness Mar	H	H

## Example 3

### Preparation of Pigmented Acrylated Epoxy Powder Coating With Dual Thermal and UV Cure

The ingredients listed below in Table 3A were compounded as described to form a pigmented powder coating of

this invention having a dual cure, thermal and UV, aspect.

### Comparative Example 3

#### Preparation of Pigmented Acrylated Epoxy Powder Coating With Peroxide Cure Only

The ingredients listed below in Table 3A were compounded as described to form a pigmented powder coating having a thermal peroxide cure aspect only.

Table 3A

Ingredients	Phr	
	Example 3	Comp. Ex. 3
DRY BLEND UNTIL HOMOGENEOUS		
Pro 1723 Unsaturated Polyacrylate <sup>1</sup>	100	100
Lupersol 231XL Peroxide	5.0	5.0
TiPure R-960 Titanium Dioxide	20	20
Resiflow P67 Acrylic Flow Aid	1.4	1.4
Benzoin	0.8	0.8
Benzyl Dimethyl Ketal Photoinitiator	2.0	0
Total	129.2	127.2
CHARGE TO EXTRUDER AND EXTRUDE TO SHEETS		
MELT TEMPERATURE = 180°F		
AIR COOL AND BREAK INTO CHIPS		
CHARGE TO MILL AND GRIND TO POWDER AT HIGH SPEED		
SCREEN TO -140 MESH		

<sup>1</sup>Pro 1723 Polyacrylate is a solid epoxy acrylate resin that is available from Sartomer Company.

### Results

The powder coating compositions listed in Table 3A were electrostatically sprayed with a tribo gun on respective ½" medium density fiber boards preheated using infrared lamps to about 200°F to 250°F. The coated boards were post heated with quartz IR lamps for up to 2 minutes at about 300°F for the peroxide sample only in order to melt and cure the powder and for about 30 sec. at about 300°F for the dual cure sample in order to initiate thermal cure and form a molten film. After flow out, the dual cure sample was then cured immediately by exposure to UV radiation, first with a V-lamp and then with a H-lamp at 30 ft./min. for about one second. The cured powder coatings were subjected to performance tests with the test results listed below in Table 3B.

Table 3B

Test	Result	
	Example 3	Comp. Ex. 3
Cross Hatch Adhesion	4B	3B
Appearance	Slight Orange Peel	Slight Orange Peel
MEK Resistance (50 Double Rubs)	5 No Effect	2 Heavy Rub Off
Pencil Hardness Mar	H	B

**Example 4****Preparation of Solid Vinyl Ether Functionalized Urethane Crosslinker**

222 grams (2.0 eq.) of isophorone diisocyanate was weighed in a 0.5 liter kettle, fitted with a stirrer and nitrogen sparge. Heating and stirring was started with nitrogen flow of 30 ml/min in the presence of dibutyltin dilaurate catalyst. When the temperature reached 75°C, 52 grams of neopentyl glycol (1.0 eq.) was added over several hours. The exotherm was kept below 100°C. The adduct has a free isocyanate content of 15.6% (15.3% theoretical). At this point, 116 grams (1.0 eq.) of hydroxybutyl vinyl ether was added taken care not to let the isotherm exceed 100°C. After the addition was complete, the mixture was stirred until the free isocyanate content was below 0.3%. The non-crystallizing, amorphous solid reaction product was then discharged, cooled, and ground into powder.

**Example 5****Preparation of Solid Vinyl Ether Functionalized Urethane Crosslinker**

116 grams (1.0 eq.) of hydroxybutyl vinyl ether was charged in a 0.5 liter reaction kettle, fitted with a stirrer and nitrogen sparge. 116 grams (1.0 eq.) of isophorone diisocyanate trimer was added slowly to the kettle with gentle stirring. After addition, stirring was continued with moderate heat applied (maximum temperature not to exceed 60°C) until all of the isophorone diisocyanate trimer had dissolved. The temperature was then raised slowly to 100°C and the reaction mixture was allowed to react for 2-3 hours. At this point, the temperature was lowered to 70-75°C and tin catalyst was added. Care was taken to control the exotherm below 110°C. Mixing was continued until the free % NCO was below 0.5%. Finally the non-crystallizing, amorphous solid reaction product was discharged, cooled, ground, and then packaged.

**Example 6****Preparation of Pigmented Polyester/Vinyl Ether Powder Coating With Dual Thermal and UV Cure**

The ingredients listed below in Table 6A were compounded as described to form a pigmented powder coating of this invention having a dual cure, thermal and UV, aspect.

Table 6A

Ingredients	Phr
	Example 6
DRY BLEND UNTIL HOMOGENEOUS	
XP 3125 Unsaturated Polyester	80
Vinyl Ether Crosslinker (Example 4)	20
Lucerin TPO Photoinitiator	2.0
Irgacure 184 Photoinitiator	1.0
Lupersol 231XL Peroxide	2.0
Resiflow P-67 Acrylic Flow Aid	2.0
TiPure R-902 Titanium Dioxide	25
CHARGE TO EXTRUDER AND EXTRUDE	
MELT TEMPERATURE = 180°F	
AIR COOL AND BREAK INTO CHIPS	
CHARGE TO MILL AND GRIND TO POWDER	
SCREEN TO -140 MESH	



## Results

The powder coating listed in Table 6A was electrostatically sprayed with a tribo gun on a ½" medium density fiber board preheated using infrared lamps to about 200°F to 250°F. The coated board was post heated with quartz IR lamps at about 400°F for about 40 seconds in order to form a molten film. The molten coating was then cured immediately by exposure to UV radiation, first with a V-lamp and then with a H-lamp at 20 ft./min. for about one second. The cured powder coating was subjected to performance tests with the test results listed below in Table 6B. Due to the polymeric nature of the vinyl ether urethane crosslinkers, this powder coating had better flexibility which resulted in improved adhesion to the substrate after curing.

Table 6B

Tests	Properties
MEK Rubs (50 Double Rubs)	No Effect
Cross Hatch Adhesion	3B
Hardness Mar	HB
Pencil Gloss, 20°/60°	38/86

## Example 7

### Preparation of Pigmented Crystalline Polyester/Vinyl Ether Powder Coating With Dual Thermal and UV Cure

The ingredients listed below in Table 7A were compounded as described to form a pigmented powder coating of this invention having a dual cure, thermal and UV, aspect.

Table 7A

Ingredients	Phr
	Example 7
DRY BLEND UNTIL HOMOGENEOUS	
Pioester 313 Unsaturated Polyester <sup>1</sup>	80
ZW-3307P Vinyl Ether Crosslinker <sup>2</sup>	20
Lucerin TPO Photoinitiator	2.0
Irgacure 184 Photoinitiator	1.5
Lupersol 231XL Peroxide Initiator	2.0
Resiflow P-67 Acrylic Flow Aid	1.4
TiPure R-902 Titanium Dioxide	25
CHARGE TO EXTRUDER AND	
EXTRUDE WITH SUPERCRITICAL CO <sub>2</sub>	
MELT TEMPERATURE = 180°F	
AIR COOL AND BREAK INTO CHIPS	
CHARGE TO MILL AND GRIND TO POWDER	
SCREEN TO -140 MESH	

<sup>1</sup>Pioester 313 Unsaturated Polyester is a solid crystalline unsaturated polyester resin that is believed to be derived from ethylene glycol and fumaric acid, and that is commercially available from Pioneer Plastics.

<sup>2</sup>ZW-3307P Vinyl Ether Crosslinker is a solid crystalline vinyl ether functionalized urethane crosslinker that is derived from 4-hydroxybutyl vinyl ether and 1,6-hexamethylene diisocyanate, and that is commercially available from DSM Resins.

## Results

The powder coating listed in Table 7A was electrostatically sprayed with a tribo gun on a steel panel and heated

with quartz IR lamps at about 400°F for about 50 seconds in order to flow out the powder into a molten film. With crystalline materials, flow out tends to be better which promotes smoother coatings. After flow out, the panels were immediately passed under a 600 watt V/H UV lamp at 20 ft/min for about one second to complete the cure. The cured powder coating was then subjected to performance tests with the test results listed below in Table 7B.

Table 7B

Tests	Properties
MEK Rubs (50 Double Rubs)	No Effect
Cross Hatch Adhesion	1B
Pencil Hardness, Mar	5H
Taber Abrasion, Loss (mgs.)	23.9
Appearance	Moderate Orange Peel
Gloss, 20°/60°	55/85

### Claims

1. A dual thermal and ultraviolet curable powder coating composition, which is a composition in solid particulate form that comprises a blend of:

- a) a film-forming base resin;
- b) a second resin co-polymerizable with said base resin;
- c) a photoinitiator; and
- d) a thermal initiator,

in which said composition is curable, both on the surface and through, when exposed to sufficient thermal and then UV radiation.

2. A dual thermal and ultraviolet curable powder coating composition, which is a film-forming composition in solid particulate form that comprises a blend of:

- a) an unsaturated resin selected from unsaturated polyesters, unsaturated polyacrylates, unsaturated polymethacrylates, and mixtures thereof;
- b) a second co-polymerizable resin having a functional group selected from vinyl ether, acrylate, methacrylate, and allyl ester groups, and mixtures thereof;
- c) a photoinitiator; and,
- d) a thermal initiator.

3. A composition according to claim 2, in which said unsaturated resin is an unsaturated polyester resin derived from maleic or fumaric acid, or anhydrides thereof.

4. A composition according to claim 2 or claim 3 in which said unsaturated resin is a non-crystalline, semi-crystalline, or crystalline solid.

5. A composition according to any preceding claim in which said second co-polymerizable resin is a vinyl ether functionalized urethane prepolymer.

6. A composition according to claim 5, in which said second co-polymerizable resin is a non-crystalline solid derived from isophorone diisocyanate, neopentyl glycol, and 4-hydroxybutyl vinyl ether.

7. A composition according to claim 5, in which said second co-polymerizable resin is a non-crystalline solid derived from isophorone diisocyanate trimer and 4-hydroxybutyl vinyl ether.

8. A dual thermal and ultraviolet curable powder coating composition, which is a film-forming composition in solid particulate form that comprises a blend of:

- a) an unsaturated resin selected from unsaturated polyacrylates, unsaturated polymethacrylates, and mixtures thereof;
- c) a photoinitiator; and,
- d) a thermal initiator,

in which said composition is curable, both on the surface and through, when exposed to sufficient thermal and then UV radiation.

9. A composition according to any preceding claim which further comprises:

- e) an opacifier selected from pigments, fillers, and mixtures thereof.

10. A composition according to any preceding claim which further comprises:

- f) a catalyst.

11. A composition according to claim 10 wherein the catalyst (f) is a metal compound based on a fatty acid or oil.

12. A composition according to claim 11 wherein the catalyst (f) is a cobalt compound selected from cobalt octoate, cobalt neodecanoate, cobalt naphthenate and cobalt octadecanoate.

13. A composition according to any preceding claim in which said thermal initiator is selected from peroxide and azo compounds.

14. A composition according to any preceding claim which is curable, both on the surface and through, upon exposure to sufficient heat to melt and flow out said powder composition to a smooth molten film and activate the thermal component of the cure, followed by exposure of the molten film to sufficient UV radiation to activate the ultraviolet component of the cure and form a fully cured hardened film.

15. A method of producing a fully cured film of a radiation curable powder coating on a substrate, which comprises:

- a) electrostatically applying a radiation curable powder coating composition over a substrate, said composition being in solid particulate form that comprises a blend of:

- i) a film-forming base resin,
- ii) optional second resin co-polymerizable with said base resin,
- iii) a photoinitiator,
- iv) a thermal initiator, and
- v) optional opacifier selected from pigments and fillers;

- b) applying sufficient heat to said powder coating to melt and flow out said coating into a smooth molten film and activate the thermal component of the cure; and,

- c) applying sufficient ultraviolet radiation to said molten film to activate the ultraviolet component of the cure and form a fully cured, both on the surface and through, hardened film finish.

16. A method according to claim 15, in which said substrate is a heat sensitive substrate.

17. A method according to claim 16, in which said heat sensitive substrate is selected from wood and plastic materials.

18. A substrate having a powder coating composition according to any of claims 1 to 14 coated and cured thereon.

19. A coated substrate according to claim 18, in which said substrate is a heat sensitive substrate.

20. A coated substrate according to claim 19, in which said heat sensitive substrate is selected from wood and plastic materials.



European Patent  
Office

# EUROPEAN SEARCH REPORT

Application Number  
EP 97 31 0498

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	DE 42 28 401 A (BASF LACKE + FARBEN)  * abstract * * column 3, line 32-40 * * column 5, line 2-9 * * column 5, line 60 - column 6, line 4 * * column 6, line 21-26 * * column 6, line 46-58 *	1-3, 9, 10, 13-15, 18	C09D5/03 C09D167/06 C09D4/06
A, D	EP 0 636 669 A (DSM) * claims *	1-20	
A, D	WO 93 19132 A (DSM)  * whole document *	1-5, 9-13, 18-20	
A	EP 0 739 922 A (UCB) * page 6, line 35-40; claims 1, 18 *	1, 15, 18	
A	DE 42 28 514 A (HOECHST)  * abstract * * column 6, line 23-31 *	1-3, 18-20	TECHNICAL FIELDS SEARCHED (Int.Cl.6)  C09D C08F
A	EP 0 582 909 A (BAYER)  * page 2, line 32-51 * * page 4, line 37-56 * * page 5, line 13-16 *	1-3, 15-20	
The present search report has been drawn up for all claims			
Place of search <b>THE HAGUE</b>		Date of completion of the search <b>2 March 1998</b>	Examiner <b>Girard, Y</b>
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons &amp; : member of the same patent family, corresponding document</p>			

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